

injected into the phantom. This allows to compare measurements made by the system under test implemented with a reliable instrument such as a laboratory oscilloscope.

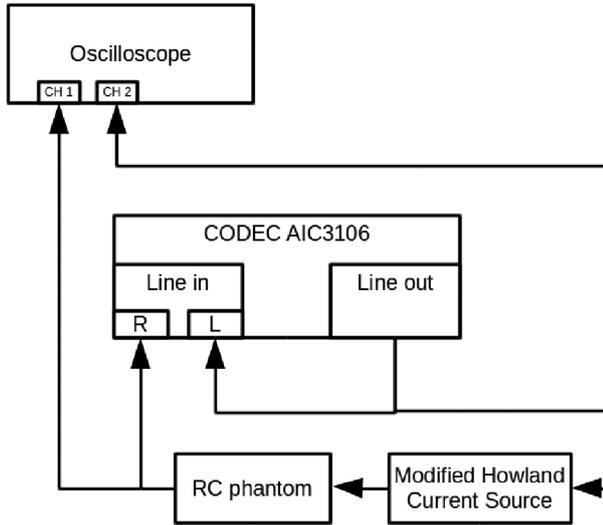


Fig. 2: Connection diagram of the test bench. The modified Howland current source feeds a phantom (parallel RC: $C = 47\text{nF}$ and a variable resistor). The oscilloscope allows to compare the original CODEC voltage signal to the phantom-shaped voltage.

The software we developed uses the phase of the reference voltage signal to compare it to the phase of the resulting phantom voltage. The output voltage signal of the phantom circuit allows to calculate the real part of the phantom impedance. We do not use the original DSP generated signal which is fed to the CODEC to control the current source, because it would introduce a lag from the time the DSP sends the signal to the time the CODEC effectively outputs the signal at its output channel. To cancel this delay we chose to use a second CODEC input channel to measure the signal of its own output port. In this way we reduce the time overhead derived from causes other than the wanted phase change between the input and output signals caused by the RC phantom.

Once sampled signals and data are sent from the CODEC to the DSP, the software routine behaves according to the diagram in Figure 3.

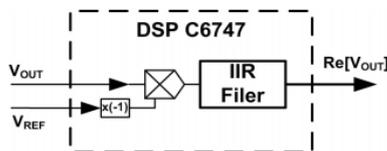


Fig. 3: DSP Implemented Synchronous Demodulator. Real part of V_{OUT} is output.

III. RESULTS

We have tested our circuit with several values of R and a fixed C value, all reported in Table 1.

Table 1: Real part of the phantom impedance.

R PHANTOM (Ω)	Impedance R/C real part @ 16KHz (Ω)	Oscil. measurement (Ω)	IMPETOM measurement (Ω)	IMPETOM adjusted R/C (Ω)	Relative Error
350	93.7	107.6	108.3	92.6	1.23%
400	87.5	111.3	104.5	88.2	0.82%
450	81.5	101.3	98.8	81.8	0.38%
500	76.0	94.7	94.6	77.1	1.43%
550	70.9	85.5	88.7	70.4	0.74%
600	66.4	78.9	84.7	66.0	0.66%
				Average Error	0.876%

Note: The first column shows the R value of the parallel RC circuit.

IV. DISCUSSION

Our previous IMPETOM designs, along with other projects, include current control by a single analog signal multiplexed into 16 current sources. When a decision was made to use digital circuits and audio kits to cut costs and ease reliable duplication of IMPETOM instruments, real part impedance measurement errors were high. Debugging gave as a result an unexpected phase lag between signals. A theoretical internal digital signal as a vector in CODEC memory was initially used as a reference to measure real world hardware signal phases. This gave rise to uncontrolled errors. By using the same CODEC generated D/A signal as a reference for measurement as well as to create the signal to submit to the “patient simulator” or phantom, reliable values were expected. This was actually the case and the present paper describes therefore the error found with the suggested circuit. An error of approximately 1% was measured, which insures a reliable enough test bench.

We found that the implemented system manages to make consistent and comparable measurements. Once the data are corrected by a linear fit to remove systematic errors in measurement, the values obtained deviate 1% on average from the expected. This shows that our system inherits the precision of a laboratory instrument. Without our system, the impedance real part would only be estimated with an error due to lack of common time reference. This special measurement is necessary because modern designs include software signal generation, as opposed to traditional layouts with a central analog oscillator to command all current sources.

V. CONCLUSIONS

We obtained a test bench that allows us to evaluate the circuit configurations for EIT design as well as for future modifications and enhancements. The ability to test the behaviour of hardware and software components on a simple phantom is a great advantage for design purposes and decision making. Several improvements can be made to the system, such as reducing the test impedance vulnerability to noise derived from the lack of electrical shielding. Additionally the inclusion of measuring bridges to improve system sensitivity should be considered. We also plan to explore the use of 32-bit digital encoding to reduce quantization errors.

VI. ACKNOWLEDGMENT

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VII. CONFLICT OF INTEREST

The authors declare they have no conflict of interest.

VIII. REFERENCES

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Author: Franco Simini
 Institute: Núcleo de Ingeniería Biomédica
 Street: Hospital de Clínicas, Av. Italia S/N, 11600
 City: Montevideo
 Country: URUGUAY
 Email: simini@fing.edu.uy